

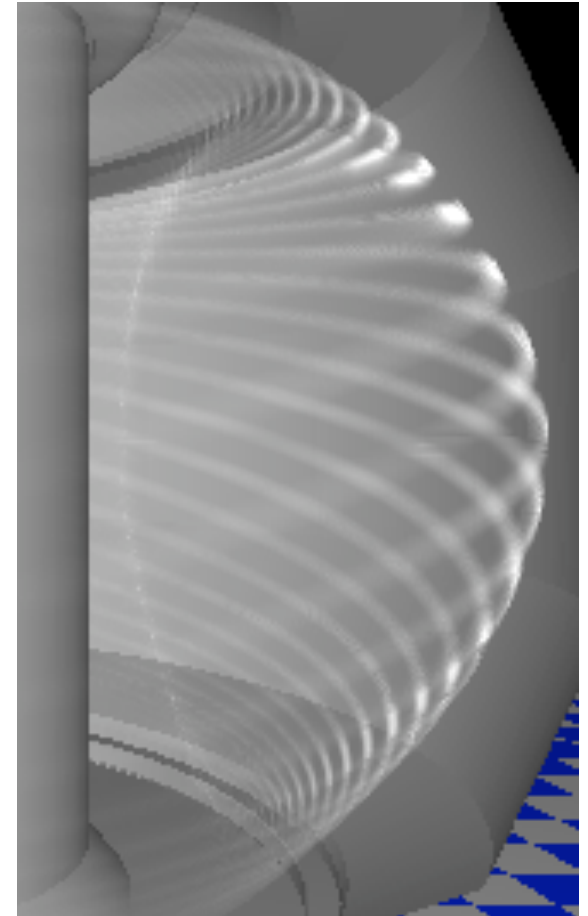
Optimizing Fusion Performance in a Tokamak: MHD, H-Mode, and AT

Philip B. Snyder

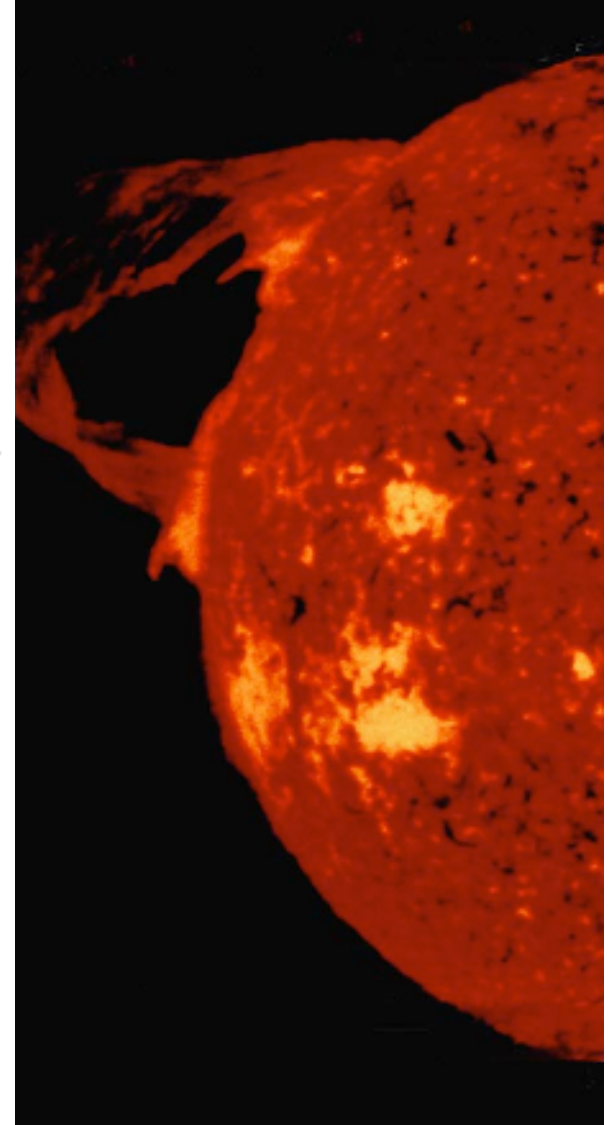
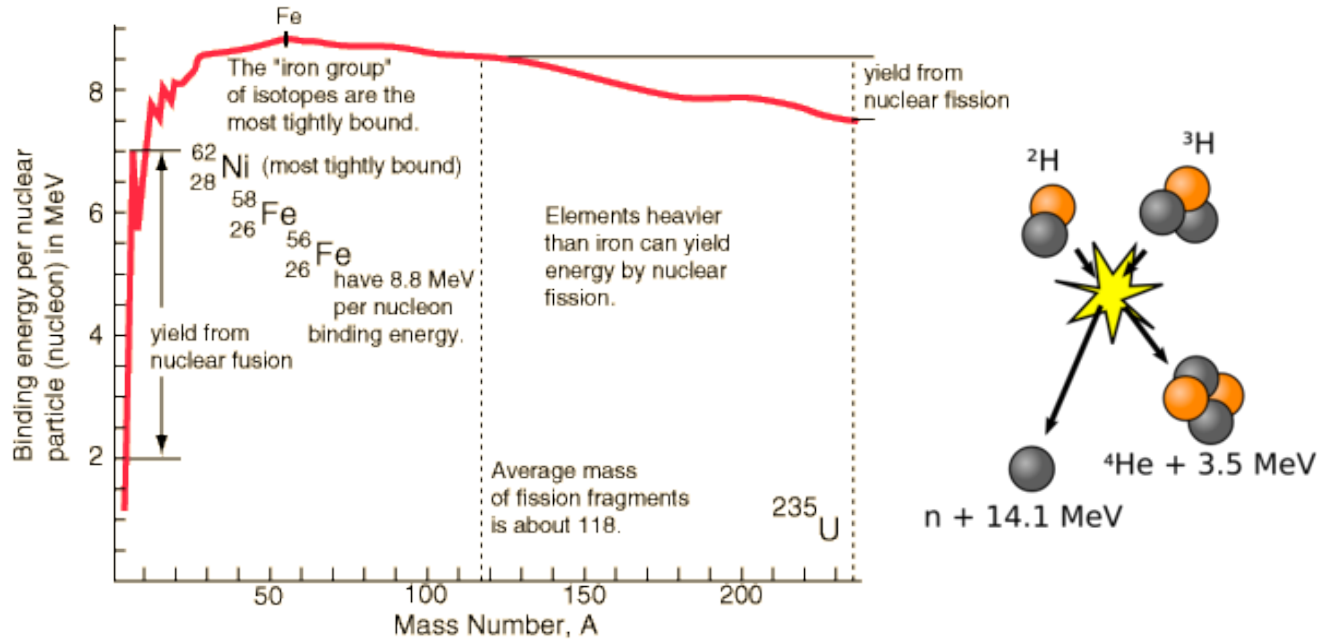
General Atomics, San Diego, USA

Acknowledgments: D. Brennan, DIII-D team

LANL Summer Student Seminar
27 July 2006



Fusion Powers the Sun and Stars



- **Light nuclei release substantial energy when fused into heavier nuclei**
 - Proton-proton and CNO fusion cycle in stars
 - D-T reaction promising for fusion energy
- **Essentially limitless supply and potentially benign environmental impact make fusion energy very appealing, despite challenges**

Basic Physics of Fusion

- **Fusion reaction rates peak at high energy (D-T ~70keV=~800 million C)**
 - High energy needed to overcome Coulomb repulsion
 - Even at peak fusion rate, cross section for fusion \ll Coulomb scattering
 - Beam-target can produce fusion, but very difficult to produce net energy gain

⇒ **Ions must be confined for several collisions**

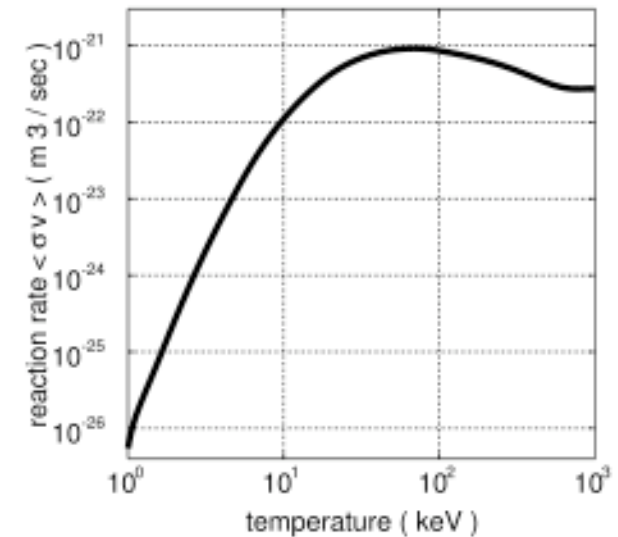
- Distribution will be approximately thermal, or Maxwellian (thermonuclear)

⇒ **At the necessary temperature, you have a plasma**

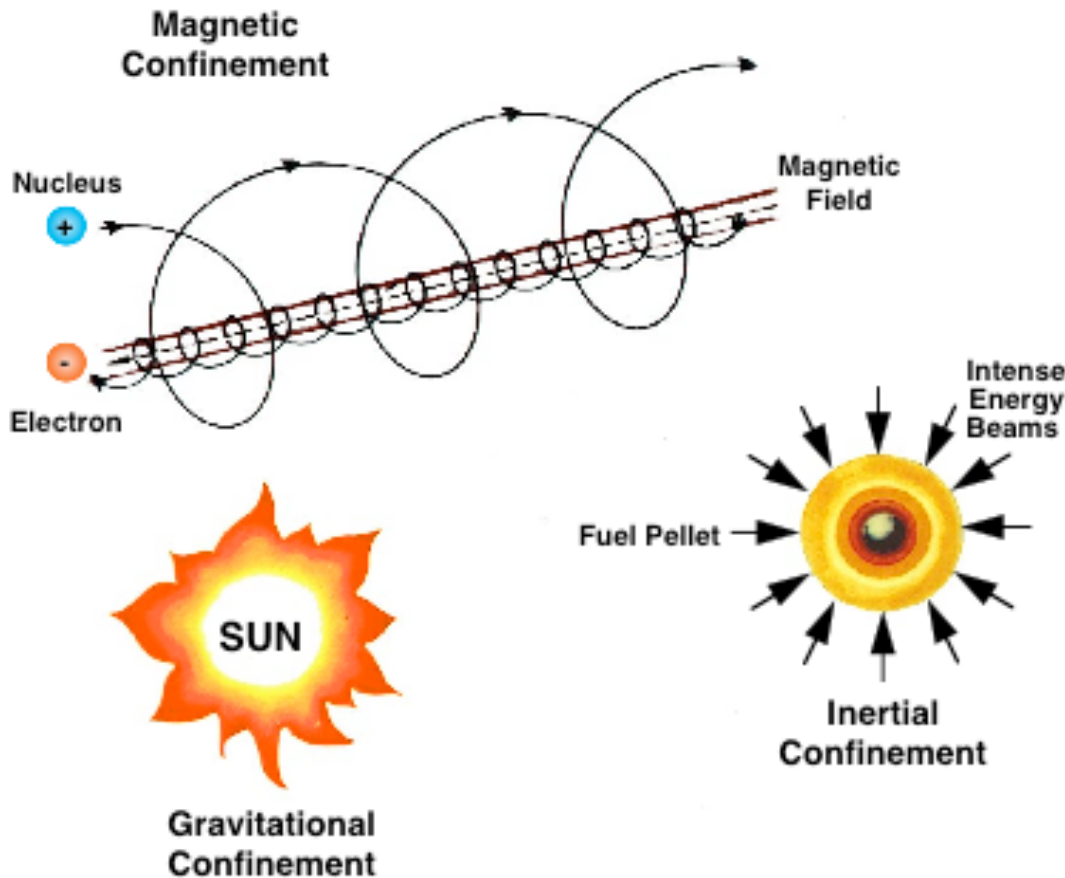
- $T \gg$ ionization energy

- **Much of the physics involved in fusion is high temperature plasma physics**

- Broad applications across many phenomena
- $> 99\%$ of universe is plasma, rocky planets are exceptions (lightning, fluorescent lights)



Approaches to Confining a Hot Plasma



- Also other variations such as electrostatic, MTF
- Here we'll focus on magnetic confinement
 - Ions follow B field lines, orbit with
$$\rho_c = v_T / \Omega_c = c \sqrt{Tm} / eB$$
 - Must close ends, magnetic mirror or...

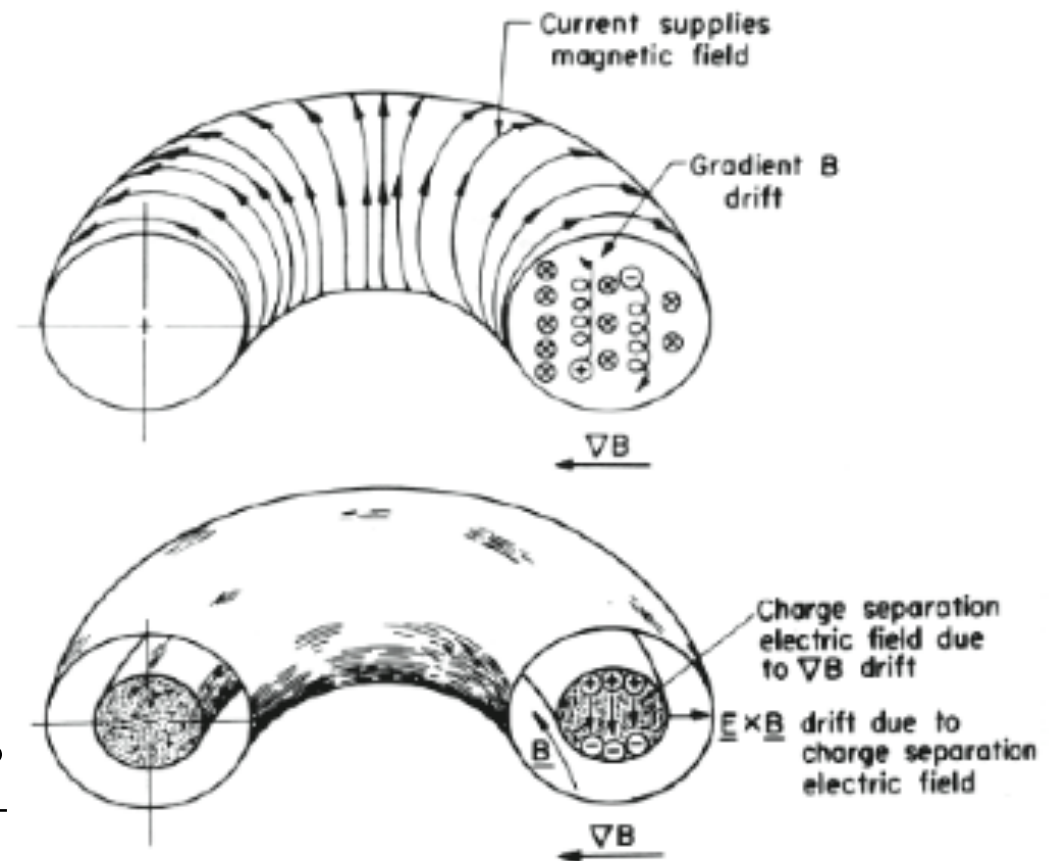
Toroidally Closed Magnetic Field Requires Helicity for Particle Confinement

$$\rho_c = v_T / \Omega_c = c \sqrt{Tm} / eB$$

With toroidal field alone the electrons and ions drift in opposite directions. A helical field prevents particle loss by averaging out the drift.

The sources of that helical field defines the different toroidal confinement devices.

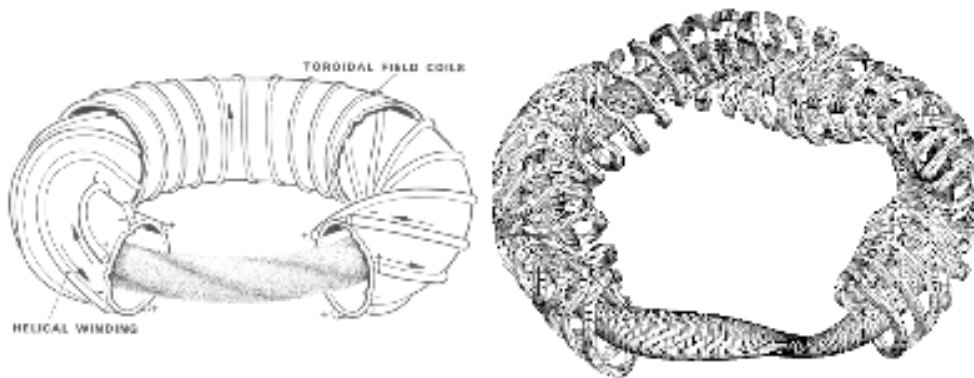
$$V_{\nabla B} = \frac{c \mu B \times \nabla B}{e B^2} \quad V_E = \frac{E \times B}{B^2}$$



Two Promising Approaches are the Tokamak and Stellarator

Stellarators have (near) zero toroidal field, and impose the helical twist externally.

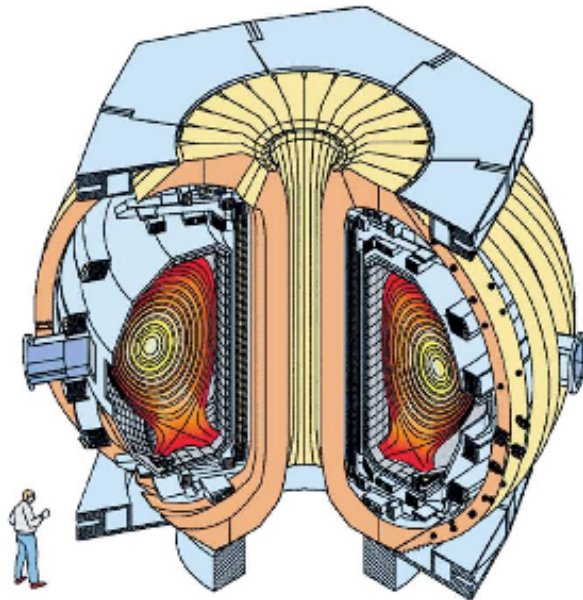
Complex coil systems.
Weak/no current driven instabilities.



Related approaches include spheromaks, RFPs, FRCs

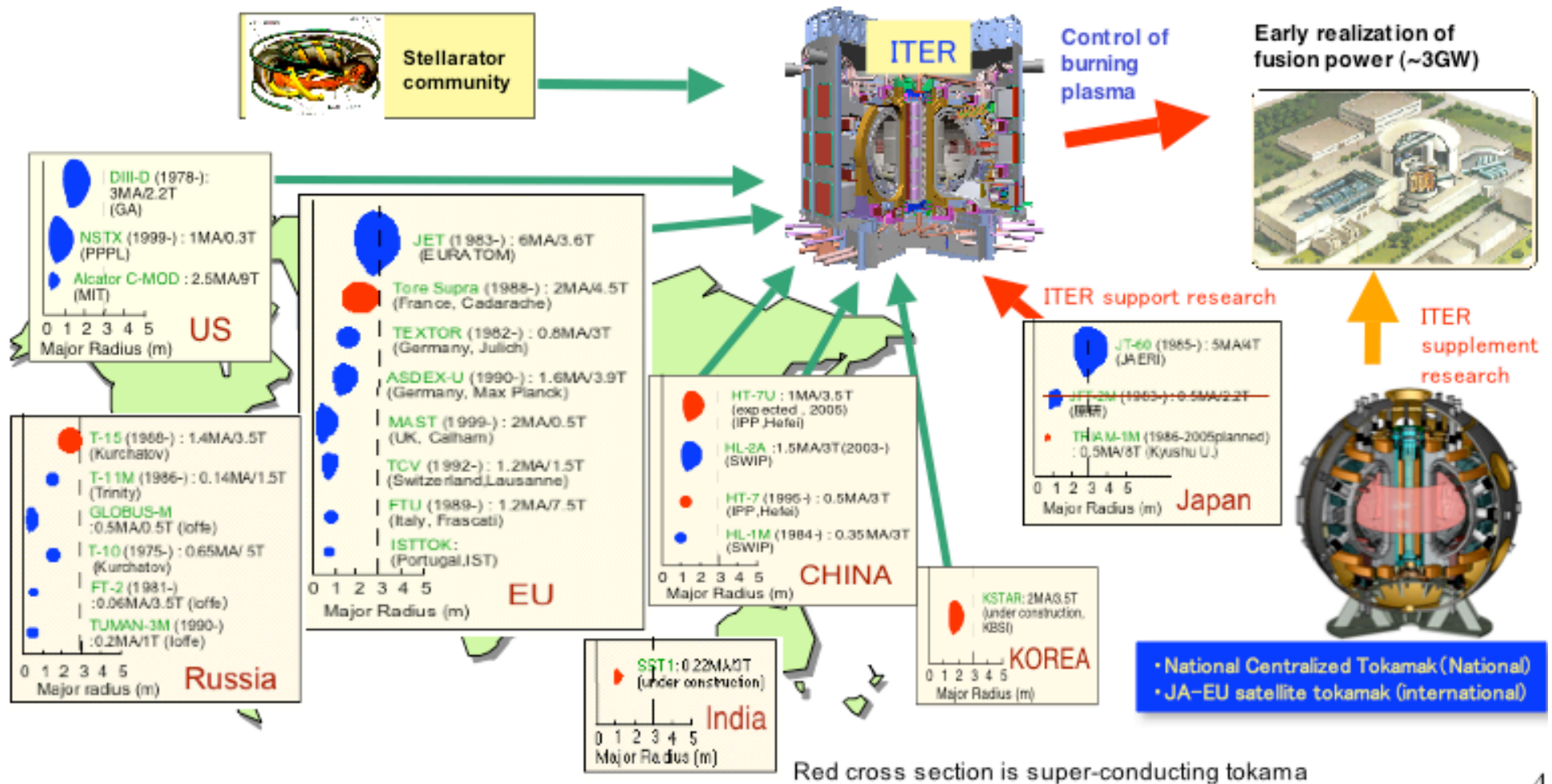
Tokamaks use a large toroidal current in the plasma to obtain the helical field.

Simple coil systems.
Current driven Instabilities.

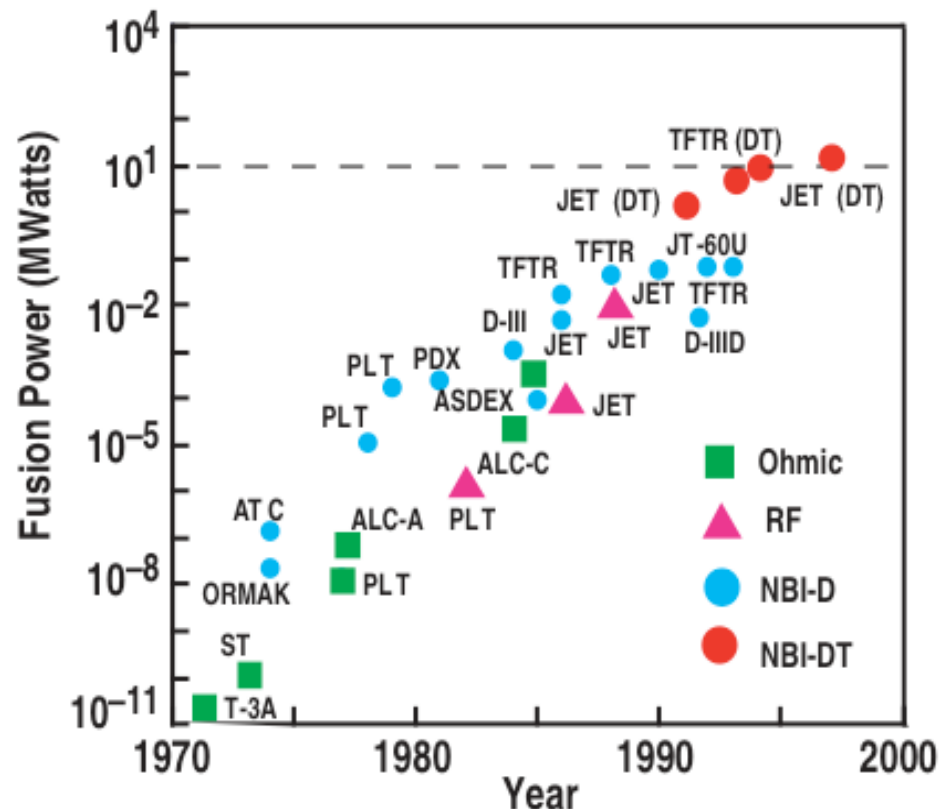


World Tokamak Research Programs

- Significant research programs in several countries
- Seven entities below partnering to focus on ITER project



Tokamak Fusion has Made Substantial Progress



- Faster than Moore's Law, approaching $Q=1$
- ITER designed for $\sim 400\text{MW}$, $Q\sim 5-10$

Optimizing Large and Small Scale Physics Key to Fusion Performance

$$\frac{P_{fus}}{P_{loss}} \propto nT\tau_E \propto B^2\beta\tau_E$$

- **Macroscopic Stability**

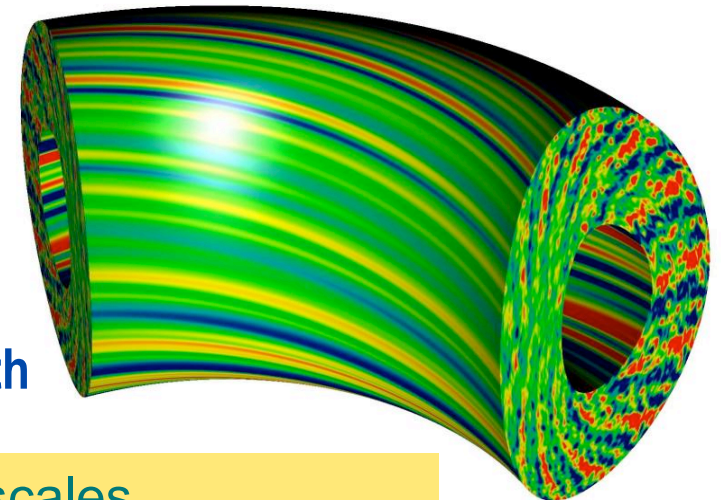
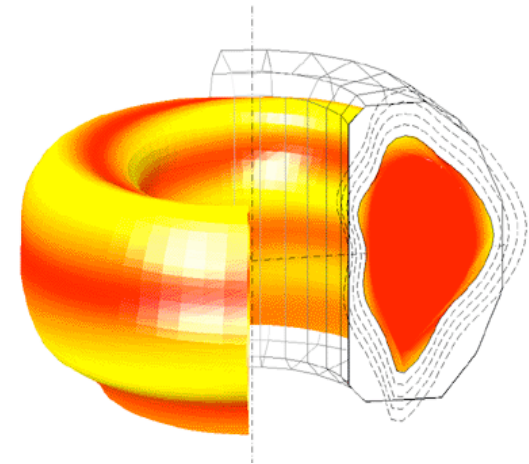
- p' and j provide free energy for MHD instabilities
- Equilibrium spatial scales
- Low n MHD codes

⇒ “ β limits” - increase with broadness of pressure profile

- **Microscopic Transport**

- Microinstabilities associated with drift motion
- Gyrokinetic theory, turbulence simulations, gyroradius scales

⇒ “Stiff transport” - roughly fixed gradient scale length



Will focus on physics at large and intermediate scales,
magnetohydrodynamics (MHD)

Outline: Physics Issues for Optimizing Tokamak Fusion Performance

- **Global pressure limits**
 - MHD physics, kink and ballooning modes
 - Resistive Wall Modes
 - Neoclassical Tearing Modes
- **H-Mode and the edge transport barrier**
 - Edge Localized Modes
- **The Advanced Tokamak**
 - Steady state, high performance

Fundamental Description of a Plasma

- **Plasma kinetic equation**

$$\frac{d}{dt} f_{\alpha}(\mathbf{x}, \mathbf{v}, t) = \frac{\partial f_{\alpha}}{\partial t} + \mathbf{v} \cdot \nabla f_{\alpha} + \frac{q_{\alpha}}{m_{\alpha}} (\mathbf{E} + \mathbf{v} \times \mathbf{B}) \cdot \nabla_{\mathbf{v}} f_{\alpha} = \sum_{\beta} C_{\alpha, \beta}(f_{\alpha}, f_{\beta})$$

- **Maxwell's equations** $\frac{\partial \mathbf{B}}{\partial t} = -\nabla \times \mathbf{E} \quad \nabla \cdot \mathbf{E} = \rho_q$

$$\rho_q = \sum_{\alpha} q_{\alpha} \int f_{\alpha} d^3 \mathbf{v} \quad \nabla \times \mathbf{B} - \frac{\partial \mathbf{E}}{\partial t} = \mu_0 \mathbf{J} \quad \mathbf{J} = \sum_{\alpha} q_{\alpha} \int f_{\alpha} \mathbf{v} d^3 \mathbf{v}$$

- **Contains all information about plasma dynamics (classical, non-relativistic)**
- **Impossible to solve analytically in any but special cases**
- **Six dimensions and wide range of spatiotemporal scales makes numerical solution impractical in all but simple cases**
- **Need to simplify for practical solution**
 - Gyrokinetics: averages over fast cyclotron timescale (5D)
 - Fluid (“MHD”): take moments of distribution functions (3D)
 - Useful for large scale physics, wide range of timescales

Deriving MHD Equations

- Define moments of distribution function

$$M_n(x, t) = \int_{-\infty}^{\infty} f(x, v, t) v^n dv$$

- Knowledge of N moments allows (in principle) reconstruction of f at N points in velocity space
- N moments of plasma kinetic equation \Rightarrow N fluid equations satisfied by M_{N+1}
 - Each additional moment equation yields more information about velocity distribution
- Use low order truncation and closures

Deriving MHD Equations

Left with series of moment equations for density, fluid velocity and temperature

$$\frac{\partial n}{\partial t} + \nabla \cdot n\mathbf{V} = 0$$

$$Mn \frac{d\mathbf{V}}{dt} = -\nabla p + \mathbf{J} \times \mathbf{B} - \nabla \cdot \Pi$$

Viscous Stress

$$\mathbf{E} = -\mathbf{V} \times \mathbf{B} + \eta \mathbf{J}$$

Resistivity

$$n \frac{\partial T}{\partial t} + n\mathbf{V} \cdot \nabla T + (\Gamma - 1)nT\nabla \cdot \mathbf{V} = -(\Gamma - 1)\nabla \cdot \mathbf{q} + (\Gamma - 1)Q$$

$$\mathbf{q} = -(\kappa_{\parallel} - \kappa_{\perp})\nabla_{\parallel} T - \kappa_{\perp} \nabla T$$

Ideal MHD omits diffusive terms, useful for studying fast, large scale instabilities

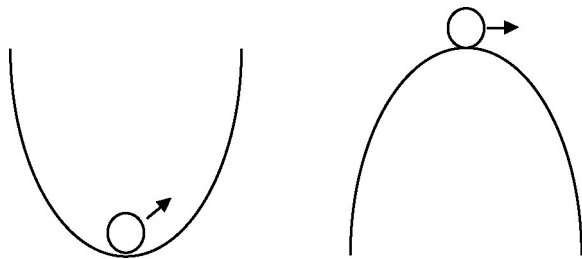
$$\frac{\partial \mathbf{B}}{\partial t} = -\nabla \times \mathbf{E}$$

$$\mu_0 \mathbf{J} = \nabla \times \mathbf{B}$$

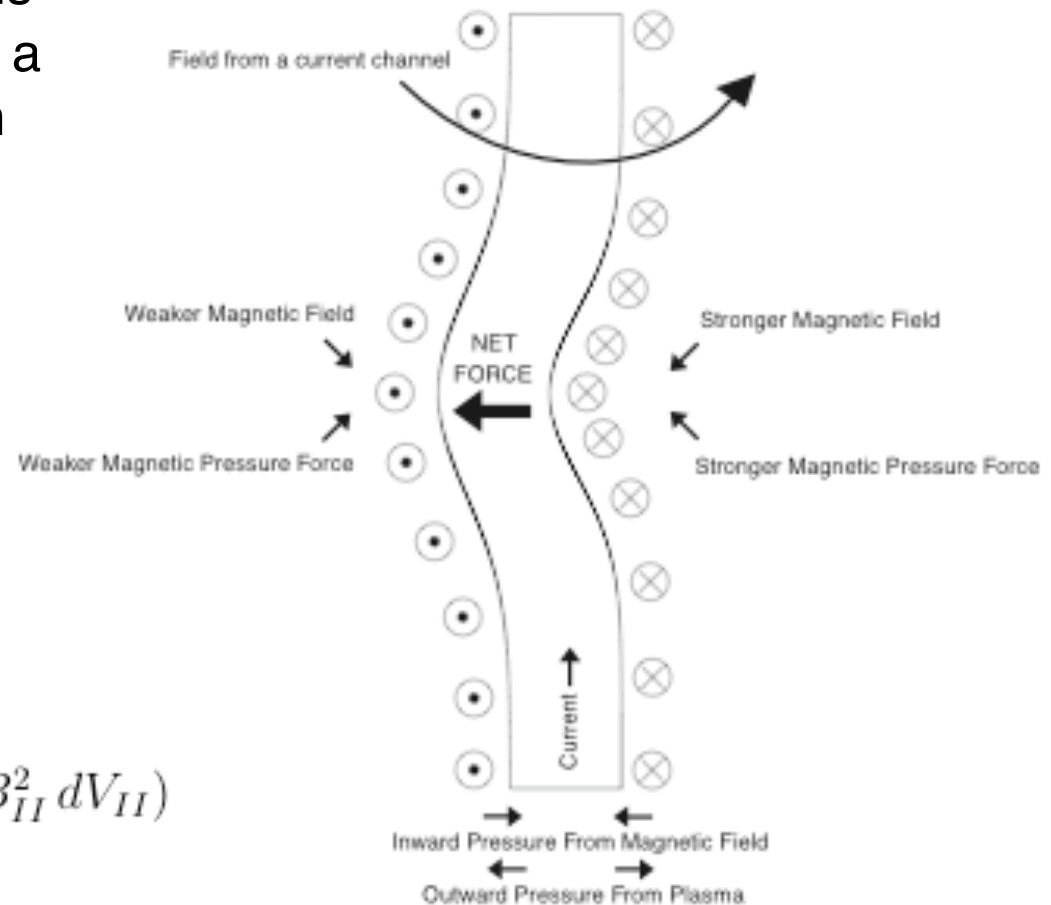
Thermal Anisotropy

MHD Instabilities

Perturbative δW method finds linear change in energy with a small perturbation; reduction is unstable.

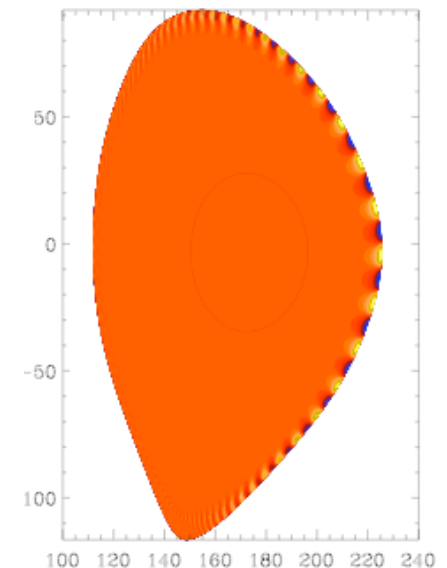
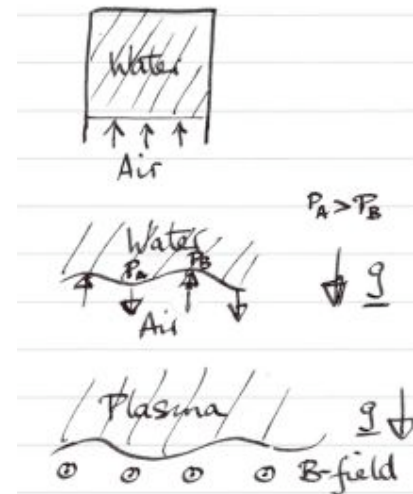
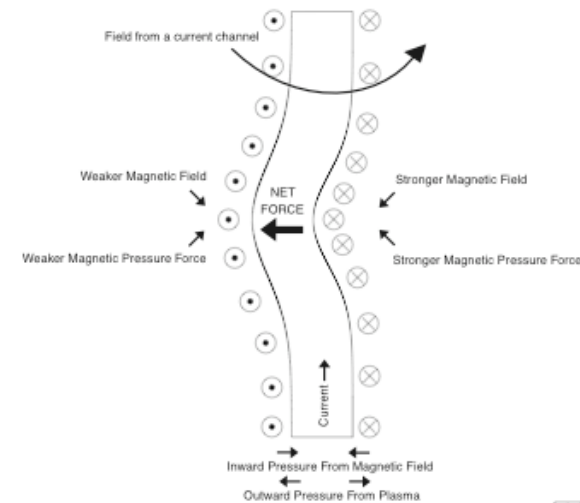


$$\Delta W = \frac{1}{2\mu_o} \left(\int_{V_I} B_I^2 dV_I - \int_{V_{II}} B_{II}^2 dV_{II} \right)$$



MHD Instabilities: Kink and Ballooning Modes

- **Current and Pressure Gradient provide large sources of free energy**
- **Kink modes are current driven**
- **Ballooning modes are pressure driven**
 - Variant of interchange mode, bad curvature
- **In practice, external kinks with both current and pressure drive often limiting**
 - Efficient numerical tools developed to calculate beta limits



Good Agreement Between Predicted and Observed MHD Beta Limits

- Numerical calculations suggest systematic β_N limit
 - Good agreement with multiple observations
- Limit increases with strong shaping and optimized profiles
- Conducting wall near plasma can stabilize modes, increase β_N limit
 - Mode that results is slow growing Resistive Wall Mode

Theory calculations (1982–1984), Troyon & Sykes

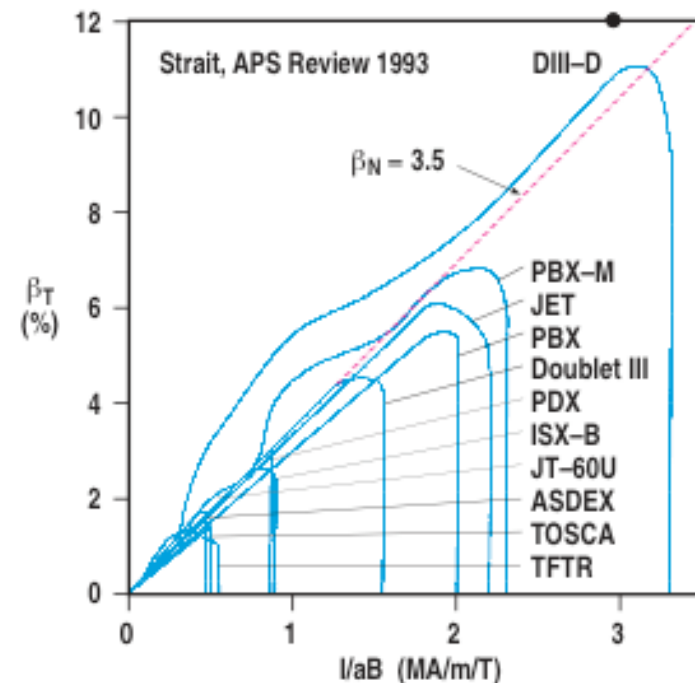
$$\beta_T (\%) \leq 2.8 \frac{I (\text{MA})}{a(\text{m}) B_T (\text{T})}, \text{ Define } \beta_N = \beta_T / (I/aB)$$

2.8 = Troyon-kink

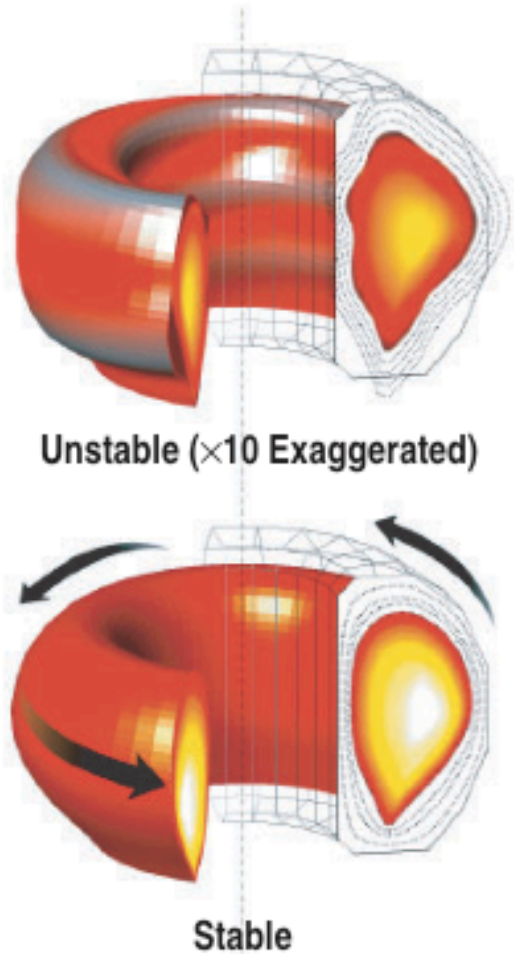
4.4 = Sykes-balloon

$$\beta_p \beta_T = 25 \left(\frac{1 + \kappa^2}{2} \right) \left(\frac{\beta_N}{100} \right)^2$$

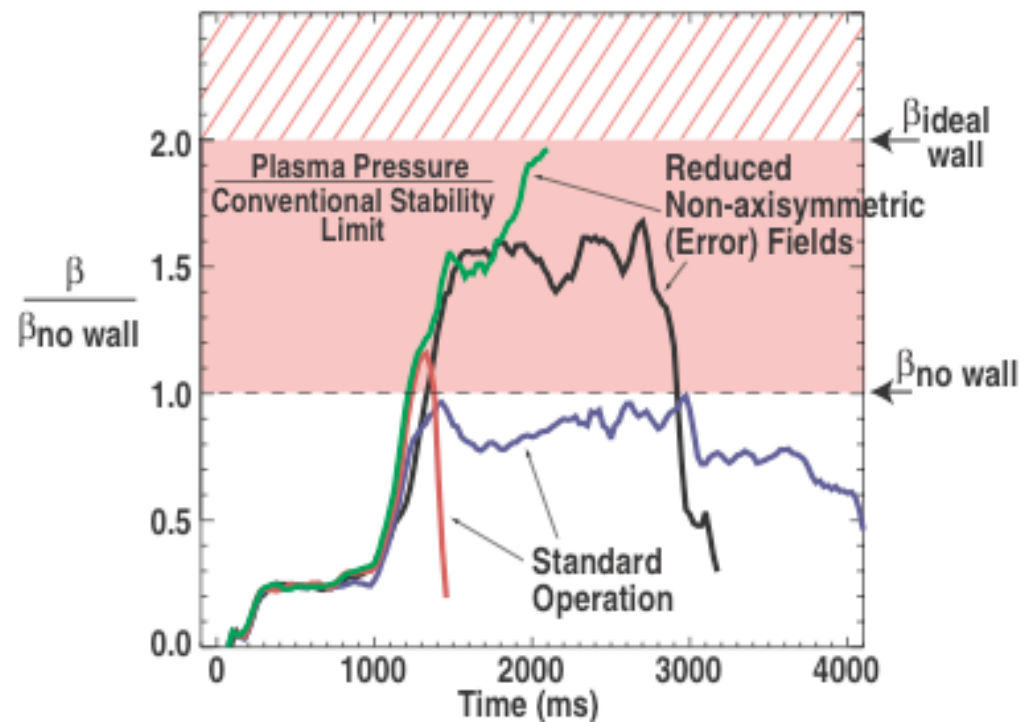
$\beta_p \beta_T$ Fusion power $\beta_T^2 B^4$
 Bootstrap fraction $c_{\epsilon}^{1/2} \beta_p$



Rapid Rotation Stabilizes RWM, allows High β Operation



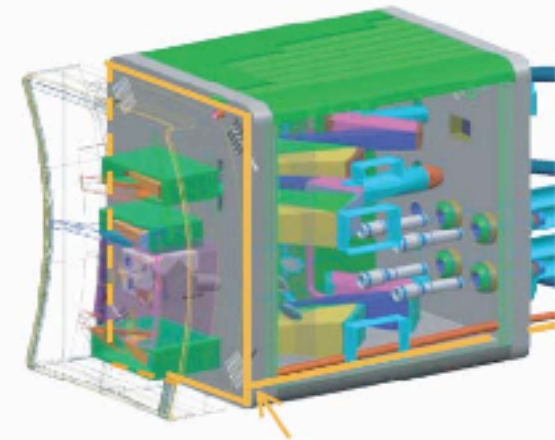
- External coils reduce error fields (reduce magnetic drag) and permit neutral beam to induce rapid rotation



Slower Expected Rotation on ITER Motivates RWM Feedback Stabilization Research

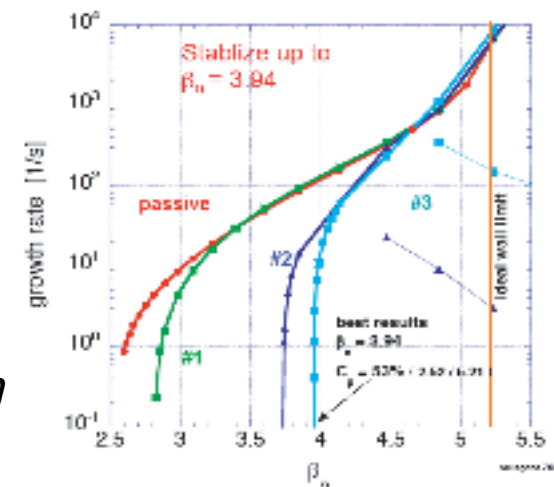
- ITER base design includes control coils
 - Error field correction: far behind vessel, blanket
 - Feedback controlled $\beta_N \approx 2.5 \Rightarrow 2.9-3.3$
- USA use in-vessel coils behind shield
 - VALEN: plasma surface current model of RWM + 3D structure circuit model
 - Blanket $\Rightarrow n=1$ ideal-wall limit $\beta_N \approx 4.5-5$
 - Feedback controlled $\beta_N \approx 2.5 \Rightarrow 4$

RWM Coil Concept for ITER



Coil behind shield module

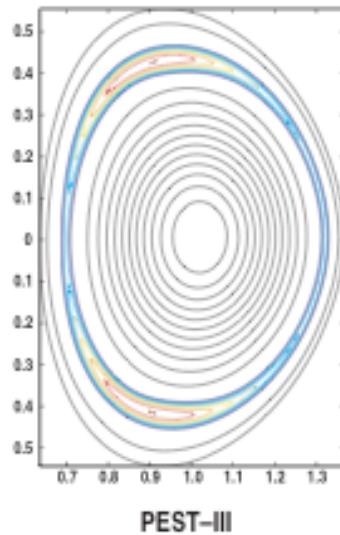
7 RWM Coils mounted behind the blanket in every other port except NBI ports. (assumes 9 ms time constant for each blanket shield module)



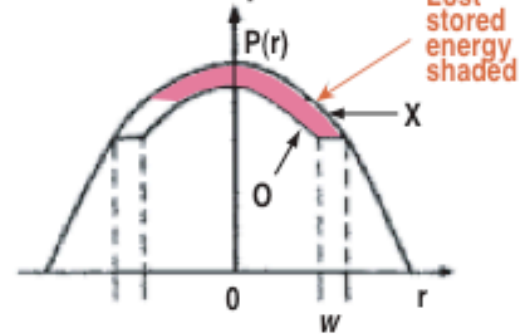
Preliminary result: Successful RWM feedback stabilization on DIII-D last week (turned neutral beam around to allow low rotation)

Magnetic Reconnection leads to Tearing Modes which can Limit β below Ideal values

Island Formation at Rational Surface



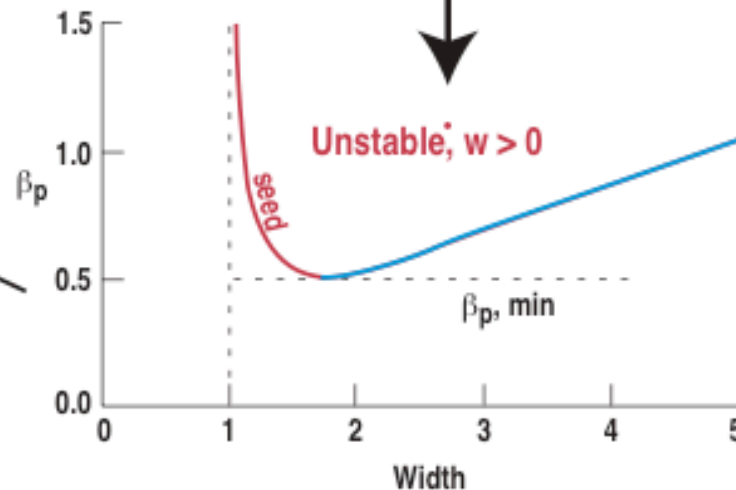
Helically Perturbed Pressure and Bootstrap Current



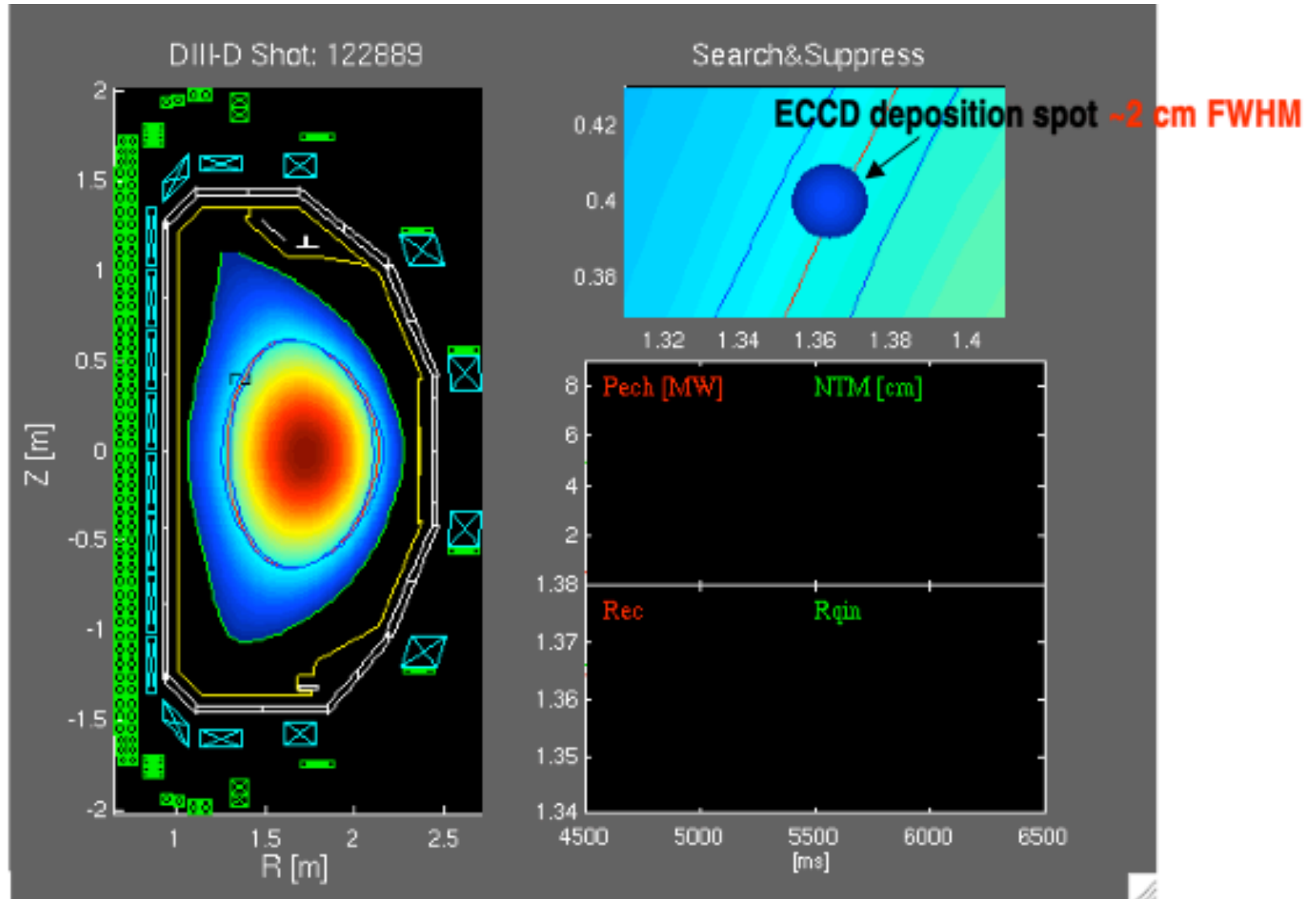
Any Significant Seed Island Leads to Limit on Achievable β

◆ Choices if High β Desired:

- Avoidance
- Stabilization



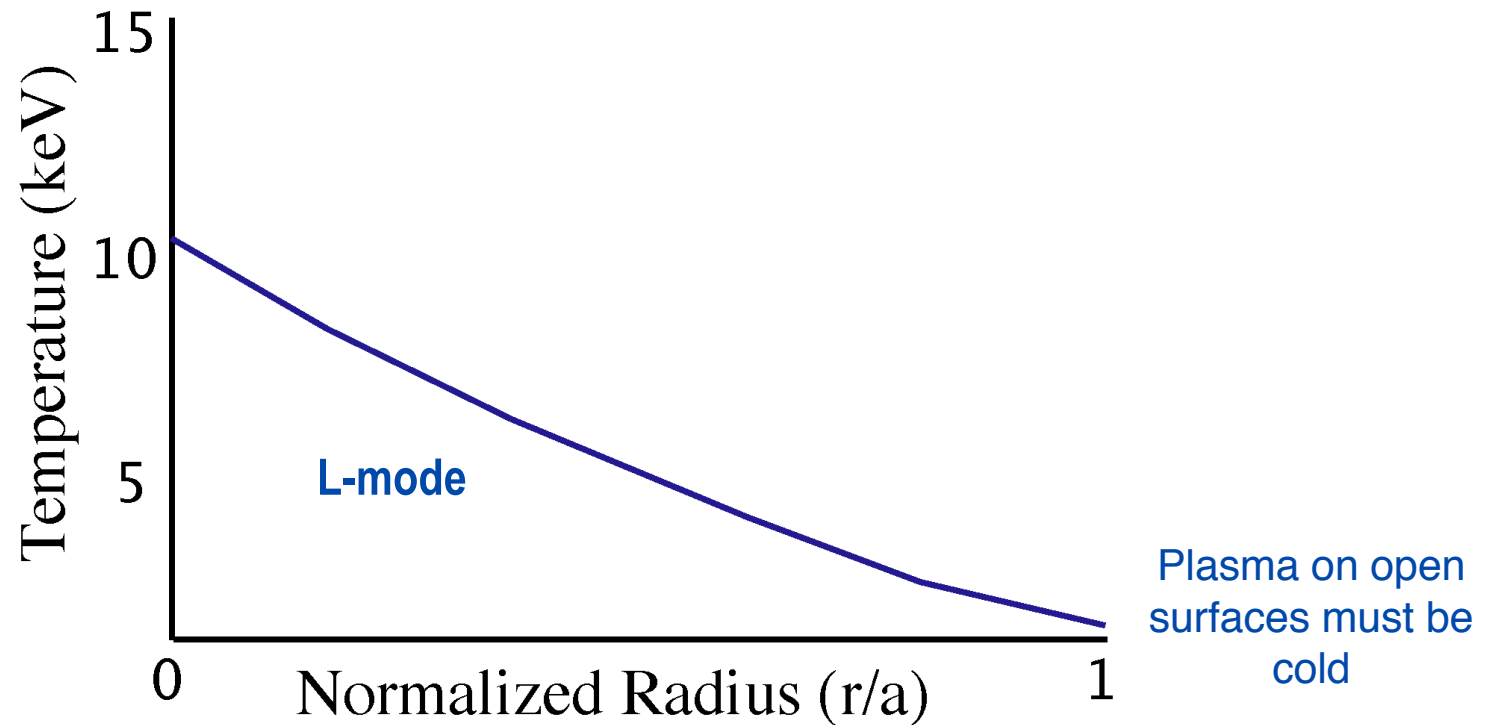
NTMs Can Be Stabilized Via Carefully Aimed Driven Current



Outline: Physics Issues for Optimizing Tokamak Fusion Performance

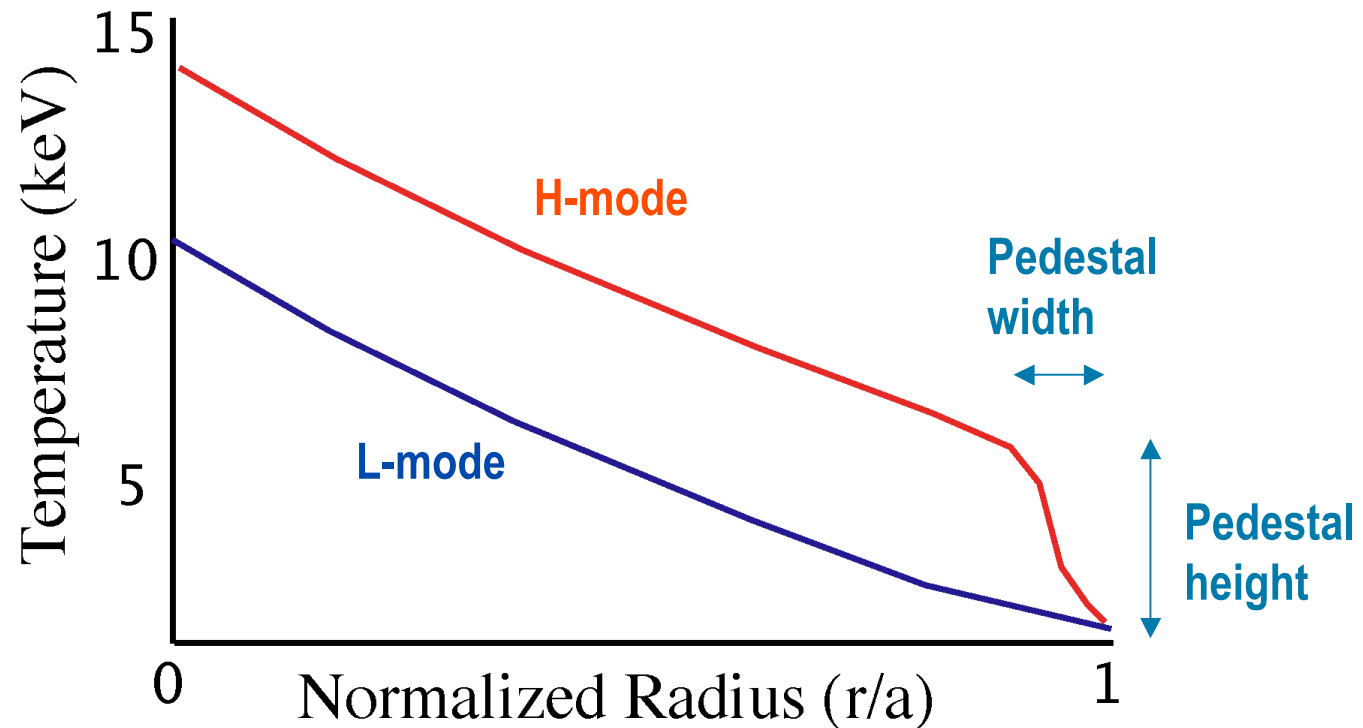
- **Global pressure limits**
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High Performance via the Edge Transport Barrier



- **Stiff transport implies approximately fixed gradients in core**
 - L-mode: Better confinement requires bigger machine (\$\$\$)

High Performance via the Edge Transport Barrier



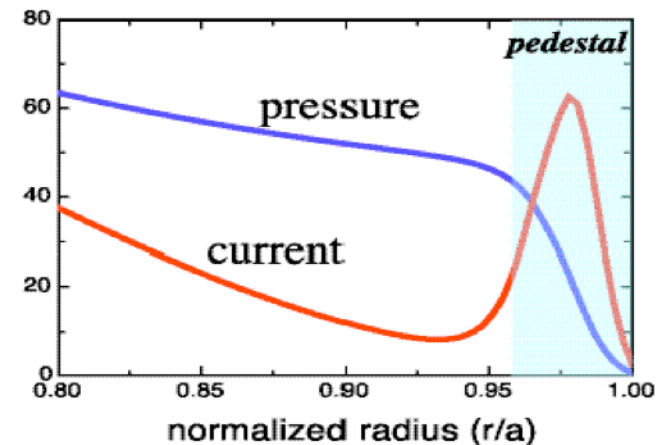
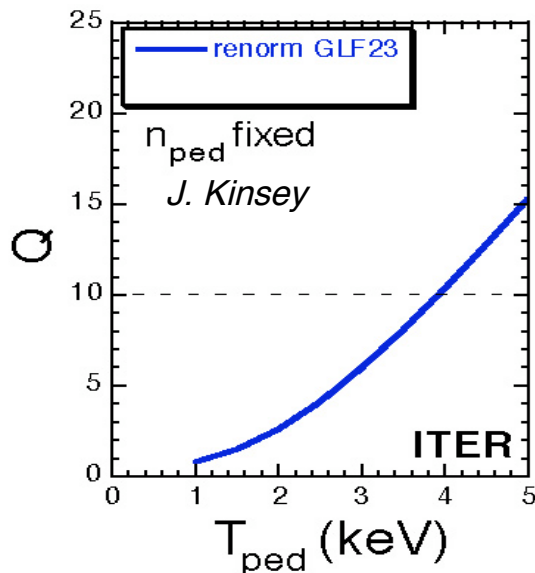
- **Stiff transport implies approximately fixed gradients in core**
 - L-mode: Better confinement requires bigger machine (\$\$\$)
- **H-mode pedestal lifts whole profile (dramatic for fixed scale length)**
 - Profile broadening raises MHD beta limit
 - “Height” of the pedestal key to performance

H-mode is reference operating mode for ITER and projected fusion reactors

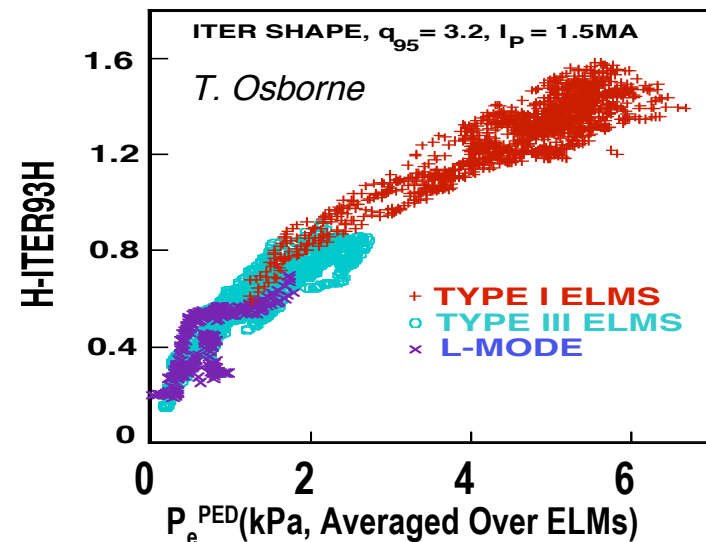
Physics of the Pedestal and ELMs

- ELMs and the edge pedestal are key fusion plasma issues
 - “Pedestal Height” strongly impacts core confinement and therefore fusion performance (Q)
 - ELM heat pulses impact plasma facing materials
 - *Both very high priority for ITER*

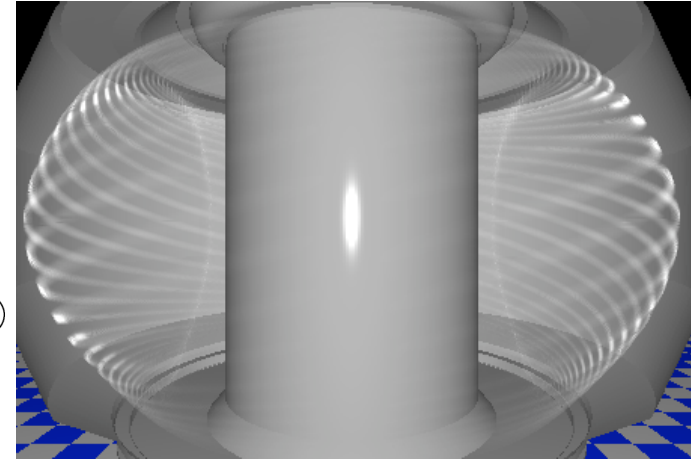
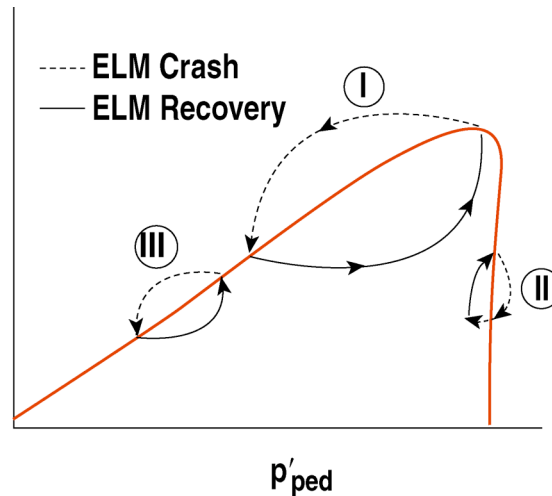
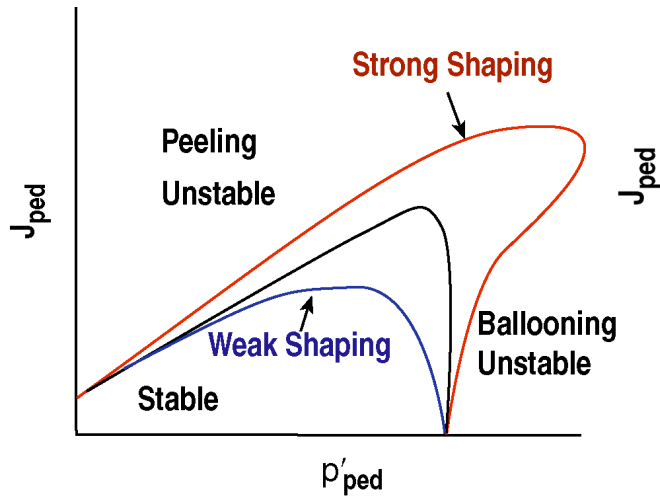
Predicted Impact of Pedestal Height



Observed Impact of Pedestal Height



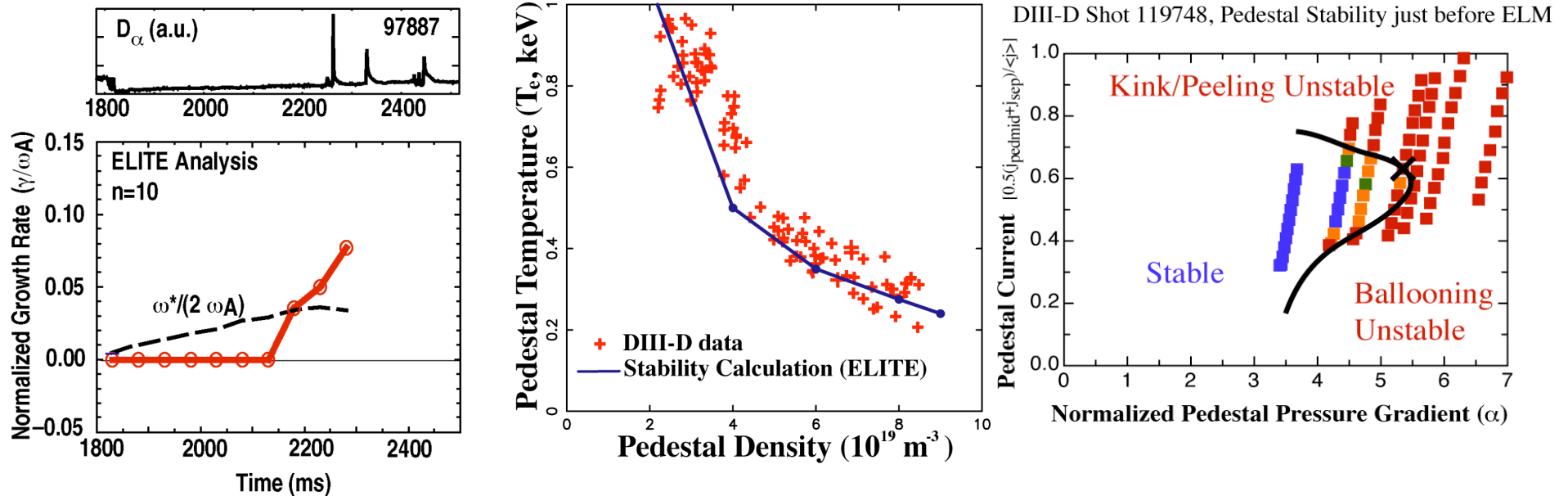
The Peeling-Ballooning Model



$n=18$ mode structure

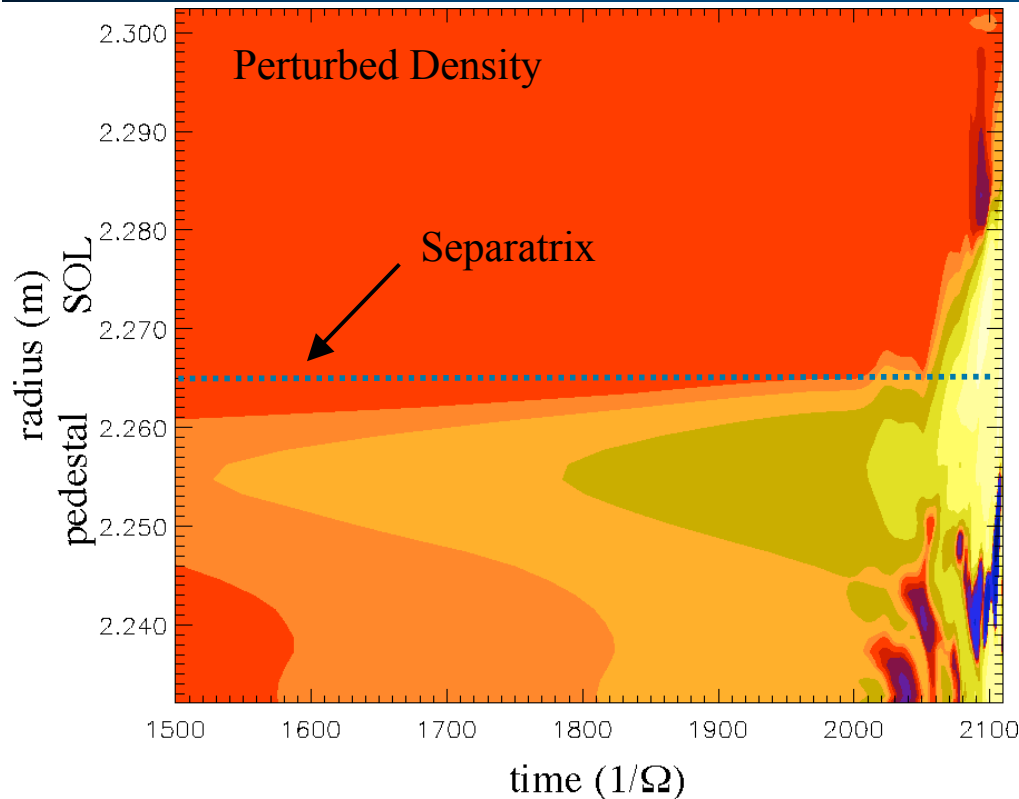
- **ELMs caused by intermediate wavelength ($n \sim 3-30$) MHD instabilities**
 - Driven by pressure gradient and current in the edge transport barrier region
 - Complex dependencies on v_* , shape etc. due to bootstrap current and “2nd stability”

The Peeling-Ballooning Model: Validation

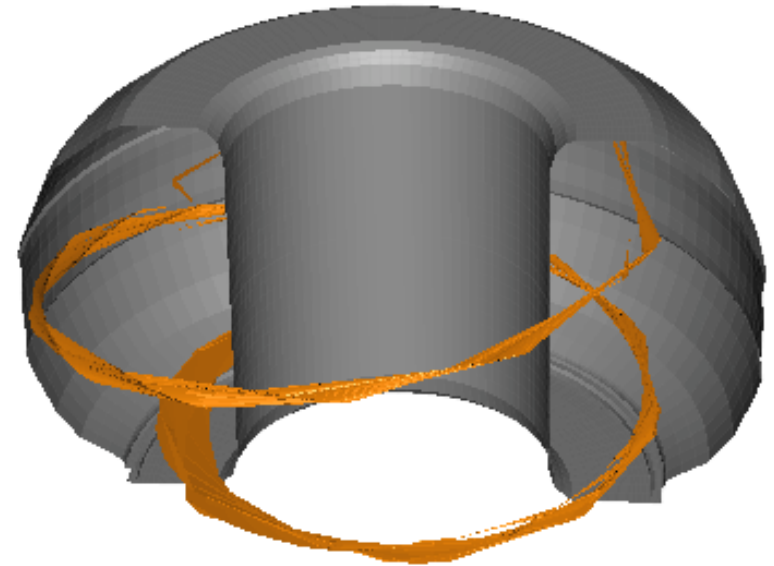


- **Successful comparisons to expt both directly and in database studies**
- **MHD physics, taking into account two fluid effects, does a remarkably good job of accounting for ELM onset and observed pedestal constraints**
 - Allows performance projections for ITER, though barrier width remains a significant uncertainty

Nonlinear Simulations of ELMs Exploring Evolution and Heat Deposition

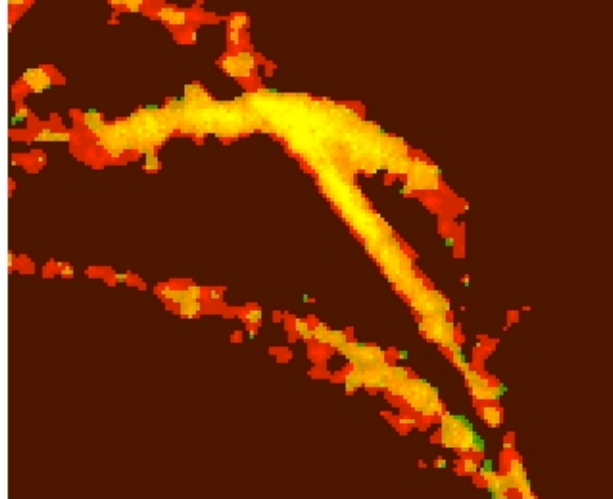
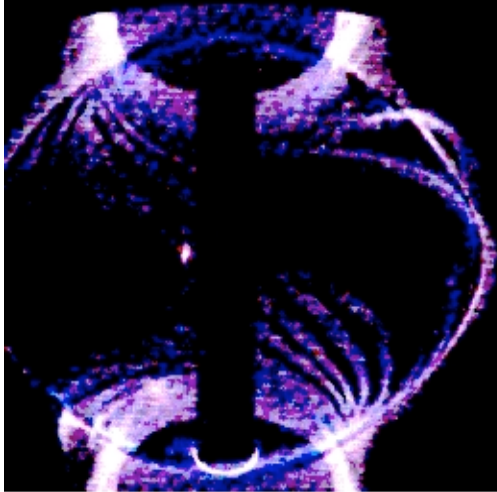


$t=2106$, surface of constant δn



- Initial linear growth phase ($n \sim 20$, $\gamma/\omega_A \sim 0.15$), then fast radial burst begins at $t \sim 2000$, can see positive density (light) moving into SOL and negative perturbed density near pedestal top
- Radial burst has filamentary structure, extended along B

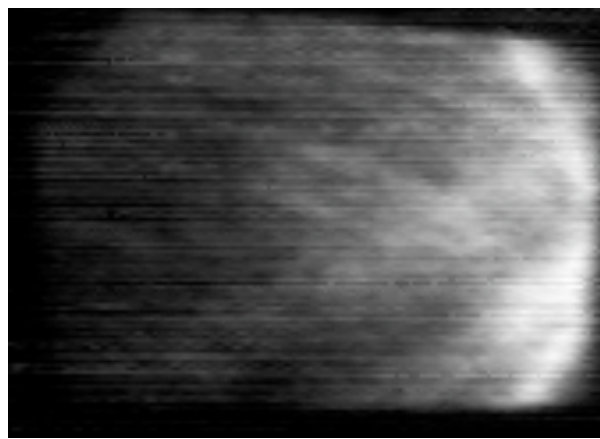
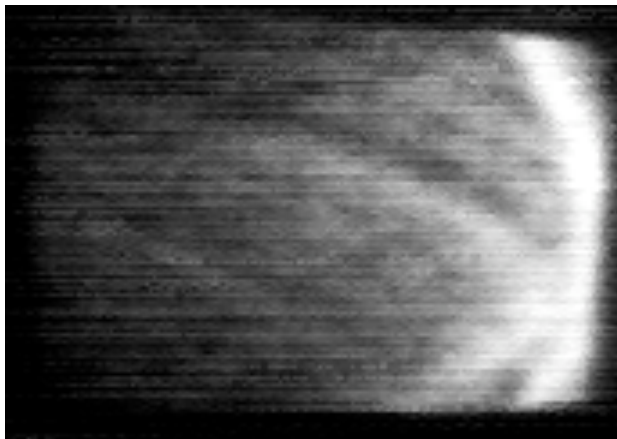
Fast ELM Observations



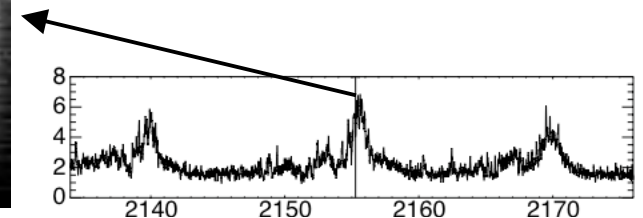
- $n=10$ structure on outboard side
- Filaments moving radially outward

A. Kirk, MAST, PRL 92 (2004) 245002-1

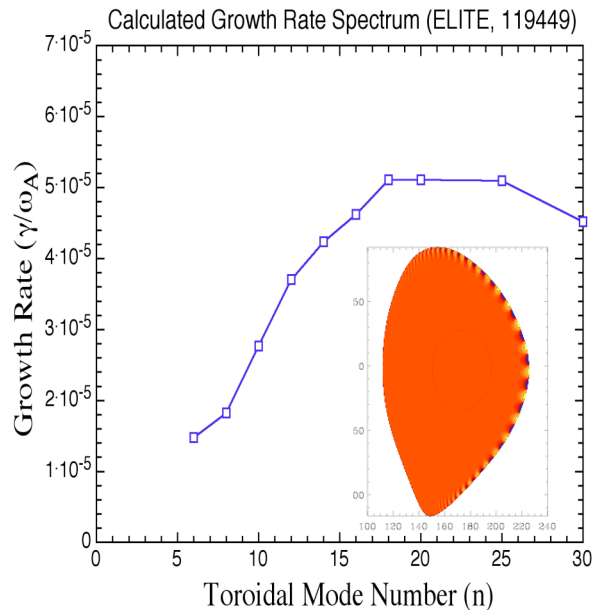
M. Fenstermacher, DIII-D, IAEA 2004



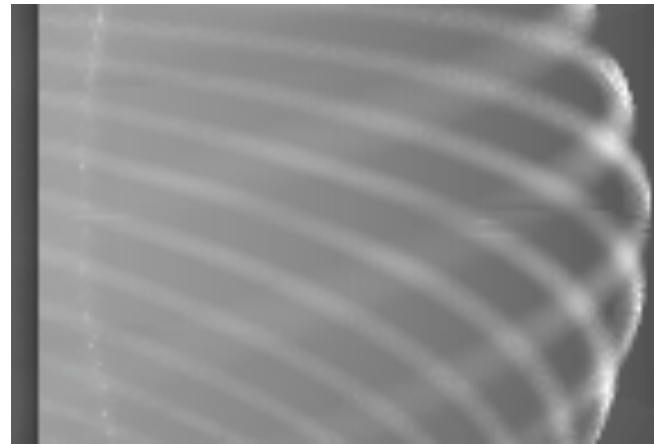
- CIII images from fast camera on DIII-D
- $n \sim 18$ inferred from filament spacing



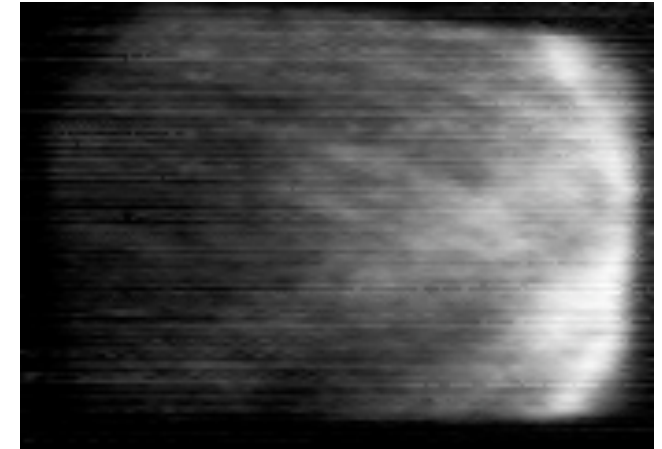
DIII-D ELM Images Compared to Simulations



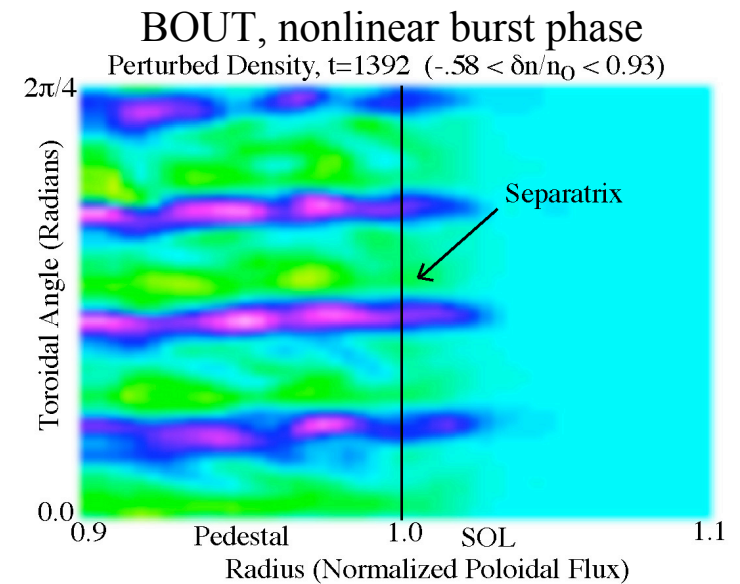
ELITE, $n=18$



Fast CIII Image, DIII-D 119449
M. Fenstermacher, DIII-D/LLNL

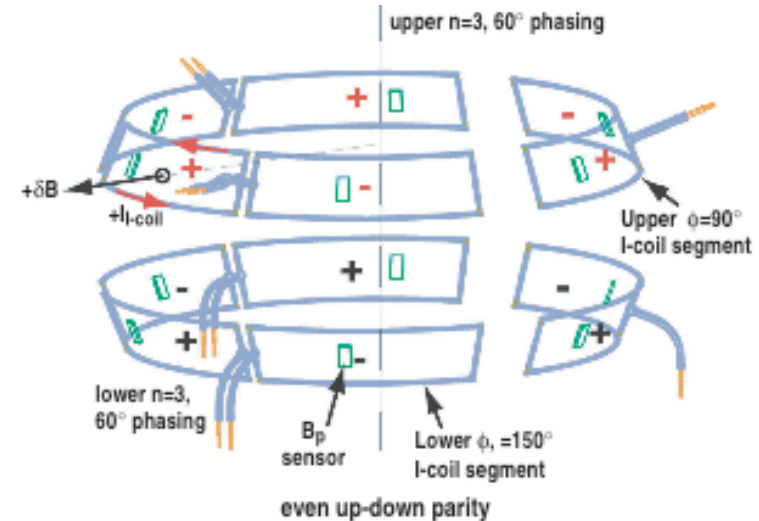
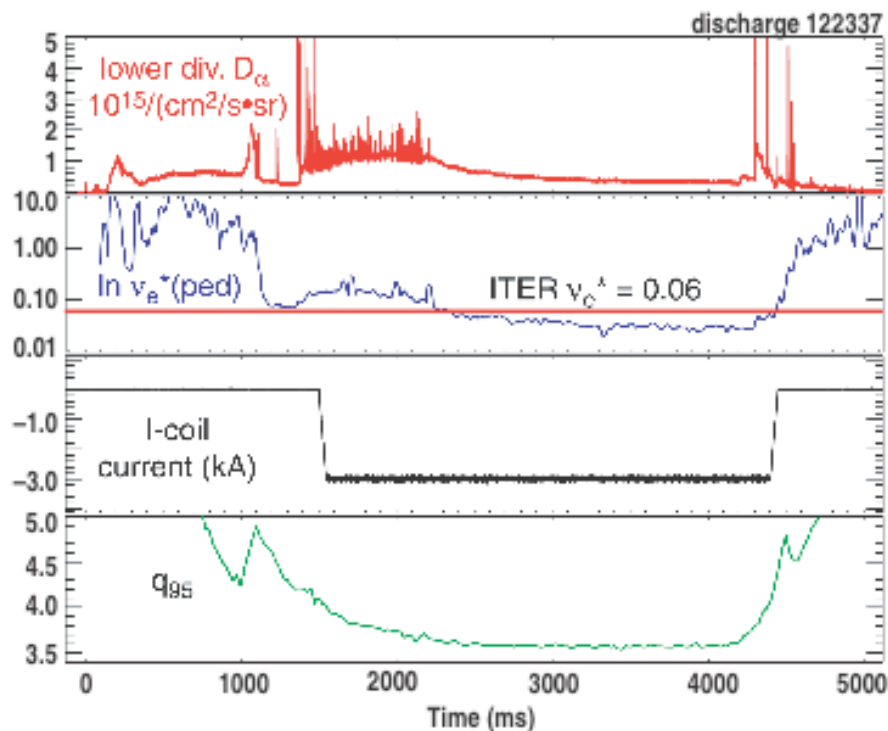


- ELITE linear P-B calculations show peak $15 < n < 25$; mode in this range predicted to be first to go unstable
- Calculated $n=18$ structure qualitatively similar to observations
- Nonlinear simulations show symmetric structure in early phase, extended uneven filaments later



ELMs Successfully Suppressed Using Non-Axisymmetric Magnetic Perturbation

- $n=3$ magnetic field from I-coil perturbs plasma edge



- No degradation in core confinement or increase in core radiation

Pedestal pressure held below ELM stability limit

Transport physics not fully understood: Not simple stochastic transport

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The Advanced Tokamak Concept Allows High Performance, Steady State Operation

- **Conventional Tokamak**

- Current is inductively driven (pulsed operation)
- Low β ($\beta_N \sim 2$), L-Mode confinement (no pedestal)
- Large machine required for power plant (\$\$)

- **Advanced Tokamak (AT)**

- Current is non-inductively driven (steady state)
 - Substantial fraction is self-driven bootstrap current
- High β ($\beta_N > \sim 4$), H-Mode or better confinement (high pedestal)
- Compact, high duty cycle power plant

High β_N is Key to Success of Advanced Tokamak

- High β is essential for high fusion power in a compact machine ($P_{fus} \sim V\beta^2 B^4$)
- High β ($\beta_p \sim \beta B^2/I^2$) also essential for getting a high fraction of self-driven bootstrap current ($f_{BS} \sim \epsilon \beta_p$)
 - High bootstrap fraction needed for cost-effective steady state operation
- Similar physics which allows high global β_N also allows high pedestal, which leads to good confinement
- **Optimizing normalized β_N is essential, both for high fusion performance and steady state: gains are multiplicative**

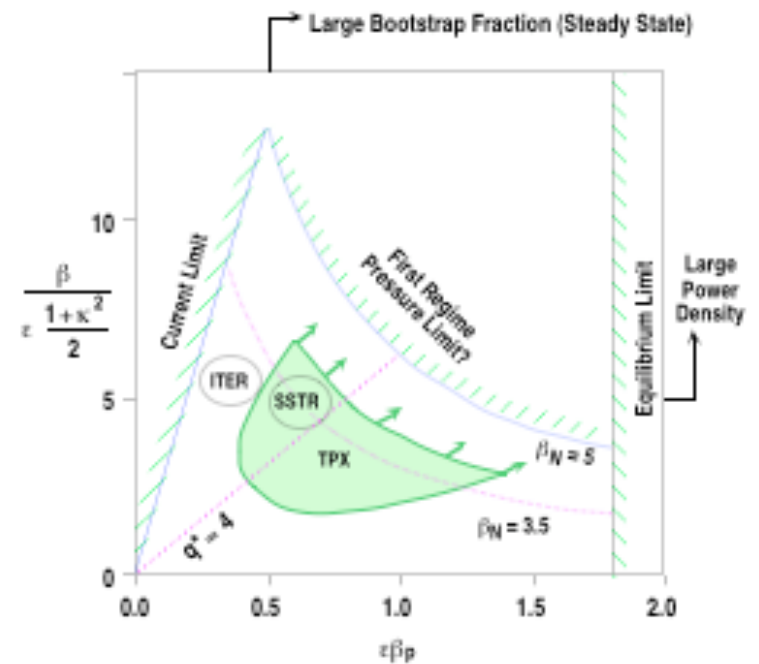
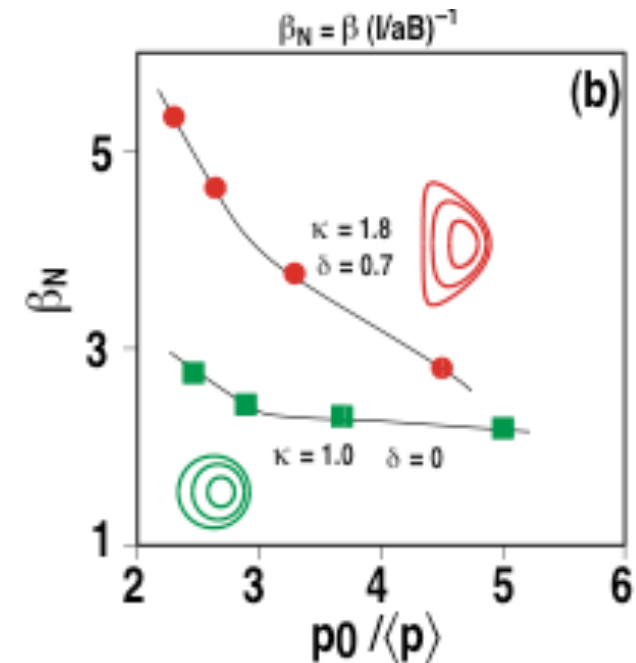


Fig. 1. A compact steady-state tokamak requires operation at high β_N . Advanced tokamak operation is toward the upper right hand corner, high β_N .

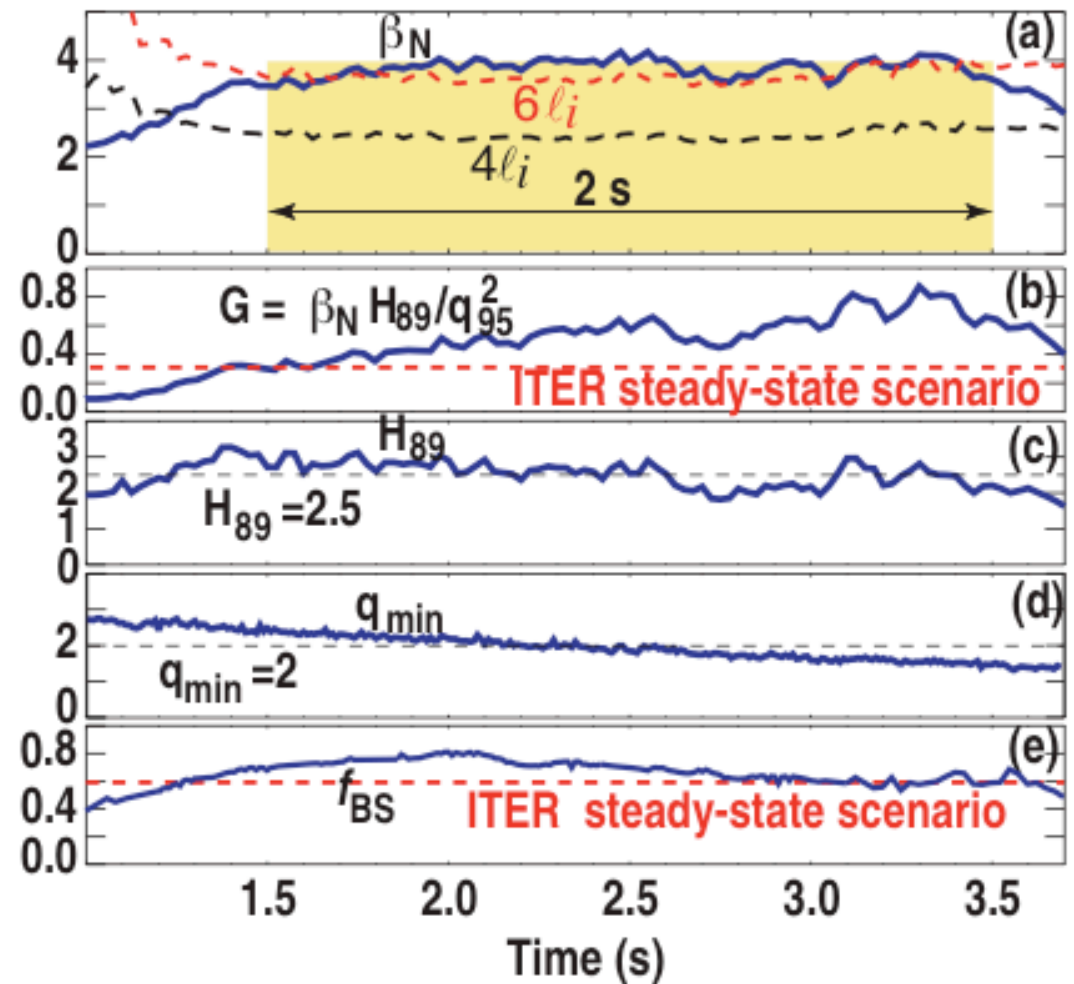
Multiple Tools and Techniques Applied to Optimize AT Performance

- **Strong shaping allows high MHD limits on global β_N**
 - Current and pressure profile optimization using neutral beams, ECCD, RF
- **RWM stabilized with rotation or active feedback**
- **NTM avoided via profile optimization or stabilized with ECCD**
- **Pedestal height optimized with shaping, ELMs mitigated with RMP or other techniques**



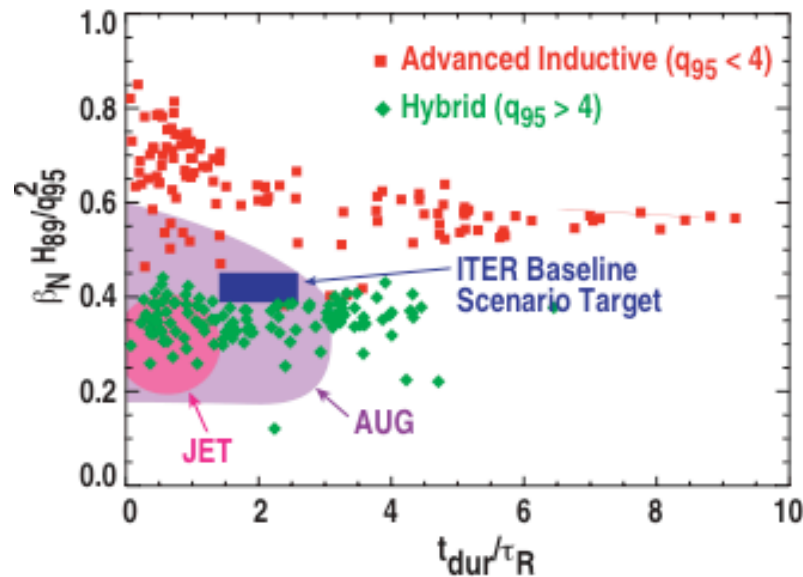
AT leads to sustained high performance on DIII-D and good projections to ITER and fusion reactors

- $\beta_N \sim 4$, $\beta_T \sim 4\text{-}7\%$
- $H_{89} \geq 2.5$
- $f_{BS} \geq 60\%$, $f_{NI} \geq 80\%$
- C-coil and I-coil used for simultaneous feedback control of error fields and RWM
- New tools in FY06–07 will help advance the understanding of RWM control
 - Balanced injection for ITER-relevant rotation
 - Additional fast amplifiers for larger control currents with low latency

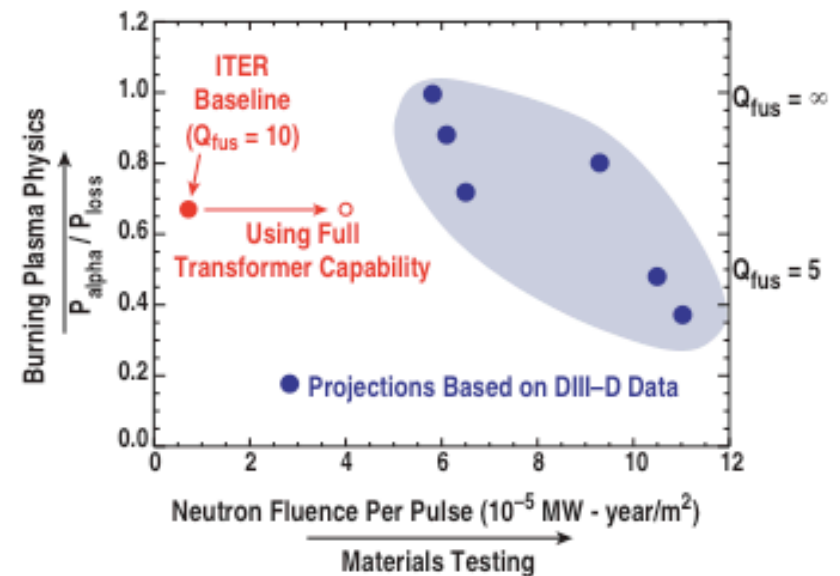


AT Regimes Project to Enhanced Capabilities for ITER and Compact Power Plant Designs

- Performance at or above ITER baseline maintained in stationary conditions



- Projections of DIII-D data suggest expanded research opportunities in ITER



- **ARIES AT reactor study projects 5c/kWh**
 - Many materials engineering and physics issues to be resolved

Summary

- **MHD physics allows understanding and control of instabilities that govern tokamak performance**
 - Kinks, ballooning modes, RWMs, NTMs, ELMs
- **Optimizing against these constraints using shaping and profile control -> high performance**
- **Doing so in steady state capable scenarios with high bootstrap current -> Advanced Tokamak**
 - High projected performance in ITER. Compact, cost-effective reactor designs possible
 - Many physics and engineering issues remain to be addressed

Sample of Key Open Issues

- **Physics (tokamak)**

- Full optimization of global beta limits (extreme shapes)
- Optimum RWM feedback control algorithm
- NTM physics at small island size
- Pedestal width and ELM suppression physics
- Optimize integrated long pulse AT operation
 - ITER required to do so at reactor-like parameters

- **Materials/Engineering (largely generic)**

- High heat flux ($\sim 10\text{MW/m}^2$), high neutron flux capable materials
 - Retain strength despite neutron activation
 - Minimize tritium retention and production of activated wastes
- Develop efficient breeding blanket technology

ITER is going forward: Will address physics and materials issues in reactor scale device

- Cost sharing settled 2003
 - ITER site decision (France) made June 28, 2005
 - Negotiation of the final agreement completed
 - “Initialing” May 2006
 - Ratification Fall 2006
 - Kaname Ikeda of Japan appointed director general November 7, 2005
 - EU, Japan, Russia, United States, Korea, China, India
-
- Opportunities to get involved both in national fusion programs and in ITER

